includes, on a mass percent basis, 0.028% of C, 0.24% of Si, 1.62% of Mn, 0.048% of Nb, 0.071% of V, 0.01% of Cu, 0.01% of Ni, and the balance being Fe and incidental impurities.

Kindly replace Paragraph [0061] on Page 15 as follows:

CH 12/5/08

[0050] Fig. 4 shows the relationship between the coiling temperature (hereinafter referred to as "CT" in some cases) and the Nb precipitation ratio. It is understood that the Nb ~~precip-itation~~ precipitation ratio is proportional to CT. When CT is more than about 700°C, the Nb precipitation ratio becomes more than about 80%. Hence, CT is preferably controlled to be about 700°C or less to obtain superior toughness. In particular, CT is preferably set to about 600°C or less.

Kindly replace Paragraph [0066] on Page 16 as follows

[0066] In contrast, according to steels I to R, which were outside ~~the invention~~ our conditions, a desired toughness could not be obtained.

Kindly replace Paragraph [0072] on Page 17 as follows:

[0072] According to our examples (steels T to X) ~~of the invention~~, it was found that the steel microstructure is composed of bainitic ferrite as a primary phase in which $\alpha B \geq 95$ percent by volume is satisfied; the strength is high such that YS $\geq$ 652 MPa is satisfied; and the toughness of the mother material and the weld portion are superior, each having a CTOD value of 0.28 mm or more.

Kindly replace Paragraph [0073] on Page 17 as follows:

[0073] In contrast, according to steel Y, since Pcm and the amount of Ca were outside the appropriate region ~~of this invention~~, the CTOD value of the weld portion was low, and the cleanness of steel was degraded by excessive addition of Ca. Consequently, a desired toughness could not be obtained.